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Optimal Runge-Kutta Schemes for High-order Spatial and Temporal Discretizations

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2015 AIAA SciTech June 23, 2015







Outline

Introduction

Governing Equations

- Spatial Discretizations
- Temporal Discretizations

Von Neumann Analysis (VNA)

Computational Results

- One-dimensional Wave
- Three-dimensional Vortex

Conclusions and Future Work



Introduction



- High-order in space is now commonplace
- High-order in time... not so much...
- Is this sufficient? Is high-order in time needed?
- Limiting Fact: There are no A-stable backward-difference formula (BDF) methods with $> 2^{nd}$ -order accuracy
- Thus, multistage methods, like Runge-Kutta (RK) methods, must be used for 3rd- and higher-order
- Explicit RK methods are not amenable to stiff problems

Objective: To find optimal diagonally-implicit Runge-Kutta time integrators for use with high-order spatial discretizations



Governing Equations



Dual Time Stepping:

$$\frac{\partial \mathbf{Q}}{\partial \tau} + \frac{\partial \mathbf{Q}}{\partial t} + \frac{\partial \mathbf{F}_i}{\partial x_i} = \frac{\partial \mathbf{V}_i}{\partial x_i} + \mathbf{H}$$

$$\mathbf{Q} = \begin{bmatrix} \rho & \rho u_i & \rho e_0 \end{bmatrix}^T$$

$$\mathbf{F}_i = \begin{bmatrix} \rho u_i & \rho u_i u_j + p \delta_{ij} & u_i \rho h_0 \end{bmatrix}^T \text{ where } h_0 = e_0 + \frac{p}{\rho}$$

$$\underline{\mathbf{A}} = \frac{\partial \mathbf{F}_i}{\partial \mathbf{Q}} = \underline{\mathbf{M}} \underline{\mathbf{M}} \underline{\mathbf{M}}^{-1}$$

$$\frac{\partial \mathbf{Q}}{\partial \tau} + \frac{\partial \mathbf{Q}}{\partial t} + \underline{\mathbf{A}} \frac{\partial \mathbf{Q}}{\partial x_i} = \frac{\partial \mathbf{V}_i}{\partial x_i} + \mathbf{H}$$

$$\underline{\Lambda} = diag\left\{u_i + c, u_i, u_i - c\right\}$$

Residual Form:

$$\frac{\partial \mathbf{Q}}{\partial \tau} + \frac{\partial \mathbf{Q}}{\partial t} + \mathbf{R}_s \left(\mathbf{Q} \right) = 0 \quad where \quad \mathbf{R}_s = \frac{\partial \mathbf{F}_i}{\partial x_i} - \frac{\partial \mathbf{V}_i}{\partial x_i} - \frac{\partial \mathbf{Q}_i}{\partial x_$$



Spatial Discretizations



Central Differences with added artificial dissipation

Central differences:

$$\left. \frac{\partial \Upsilon_j}{\partial x_i} \right|_{II} = \frac{\Upsilon_{j+1} - \Upsilon_{j-1}}{2\Delta x_i}$$

$$\left. \frac{\partial \Upsilon_j}{\partial x_i} \right|_{IV} = \frac{-\Upsilon_{j+2} + 8\Upsilon_{j+1} - 8\Upsilon_{j-1} + \Upsilon_{j-2}}{12\Delta x_i}$$

$$\left. \frac{\partial \Upsilon_{j}}{\partial x_{i}} \right|_{VI} = \frac{\Upsilon_{j+3} - 9\Upsilon_{j+2} + 45\Upsilon_{j+1} - 45\Upsilon_{j-1} + 9\Upsilon_{j-2} - \Upsilon_{j-3}}{60\Delta x_{i}}$$

where Υ could be \mathbf{F}_i or \mathbf{Q} depending on the form of the equations

Scalar artificial dissipation:

$$\mathbf{R}_{s} = \frac{\partial \mathbf{F}_{i}}{\partial x_{i}} - \varepsilon_{\eta} \parallel \lambda \parallel \frac{\partial^{\eta} \mathbf{Q}}{\partial x_{i}^{\eta}} - \frac{\partial \mathbf{V}_{i}}{\partial x_{i}} - \mathbf{H}$$

where η is even and one more than the order of accuracy

$$\|\lambda\| = |u_i| + c$$
 $\varepsilon_{II} = \frac{\Delta x_i}{2}, \quad \varepsilon_I$

$$\varepsilon_{II} = \frac{\Delta x_i}{2}, \quad \varepsilon_{IV} = -\frac{\Delta x_i^3}{12}, \quad \varepsilon_{VI} = \frac{\Delta x_i^5}{60}$$



Temporal Discretizations



Runge-Kutta Methods:

a_{1s}	a_{2s}	a_{3s}		$a_{(s-1)s}$	a_{ss}	$\overset{\circ}{q}$	b_s
$a_{1(s-1)}$	$a_{2(s-1)}$	$a_{3(s-1)}$	•••	$a_{(s-1)(s-1)}$	$a_{s(s-1)}$	$\overset{ ext{}}{\hat{b}}_{s-1}$	b_{s-1}
•	•	:		:	:	•	•
a_{13}	a_{23}	a_{33}	• • •	$a_{(s-1)3}$	$a_s 3$	\widetilde{q}^3	\vec{b}_3
a_{12}	a_{22}	a_{32}	•••	$a_{(s-1)2}$	a_{s2}	\widetilde{q}^{2}	\vec{b}_2
a_{11}	a_{21}	a_{31}	•••	$a_{(s-1)1}$	a_{s1}	$\overset{\circ}{b}_1$	b_1
C_1	C_2	C_3		C_{S-1}	C_{S}		

 $\hat{\mathbf{Q}}^{n+1} = \mathbf{Q}^n - \Delta t \sum_{j=1}^s \hat{b}_j \mathbf{R}_s^j(\mathbf{Q}^j)$ $\mathbf{Q}^{n+1} = \mathbf{Q}^n - \Delta t \sum_{j=1}^s b_j \mathbf{R}_s^j(\mathbf{Q}^j)$

 $\mathbf{Q}^k = \mathbf{Q}^n - \Delta t \sum_{j=1}^s a_{kj} \mathbf{R}_s^j(\mathbf{Q}^j)$

 $t^k = t^n + c_k \Delta t$

$$\epsilon^{n+1} = \mathbf{Q}^{n+1} - \hat{\mathbf{Q}}^{n+1}$$

ESDIRK Methods



Explicit first stage Singly-Diagonally Implicit Runge-Kutta

- Stiffly accurate
- Second-order stage accuracy
- FSAL First is the Same As Last

0	0	0		0	~	~ `	p_s
0	0	0	···	~	b_{s-1}	b_{s-1}	b_{s-1}
•	:	:	.•	:	•	•	•
0	0	~	•••	$a_{(s-1)3}$	b_3	\hat{q}^3	\vec{b}_3
0	~						
0	a_{21}	a_{31}		$a_{(s-1)1}$	b_1	$\overset{\circ}{b}_1$	b_1
$c_1 = 0$	C_2	C_3		C_{S-1}	$c_s = 1$		







ESDIRK3 and 4



0	0			1767732205903	4055673282236	1767732205903	$\overline{4055673282236}$
0	0	1767732205903	4055673282236	11266239266428	11593286722821	11266239266428	$\overline{11593286722821}$
0	$\frac{1767732205903}{4055673282236}$	640167445237	$\overline{}$ 6845629431997	4482444167858	$\overline{}$ 7529755066697	4482444167858	7529755066697
0	$\frac{1767732205903}{4055673282236}$	2746238789719	$\overline{10658868560708}$	1471266399579	$\overline{7840856788654}$	1471266399579	7840856788654
0	$\frac{1767732205903}{2027836641118}$	6	lro		Т		

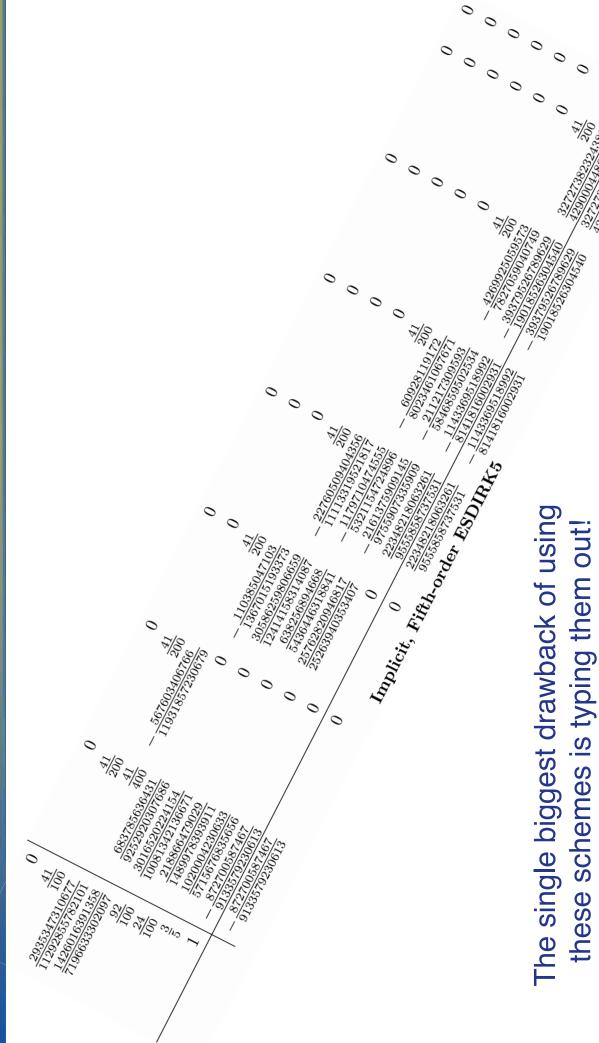
Implicit, Third-order ESDIRK3

0	0	0	0	0	114	114
0	0	0	0	114	$-\frac{2260}{8211}$	$-\frac{2260}{8211}$
0	0	0	114	$\frac{2285395}{8070912}$	$\frac{69875}{102672}$	$\frac{69875}{102672}$
0	0	114	$\frac{174375}{388108}$	$\frac{730878875}{902184768}$	$\frac{15625}{83664}$	$\frac{15625}{83664}$
0	114	$-\frac{1743}{31250}$	$-\frac{654441}{2922500}$	$-\frac{71443401}{120774400}$	0	0
0	114	$\frac{8611}{62500}$	$\frac{5012029}{34652500}$	$\frac{15267082809}{155376265600}$	$\frac{82889}{524892}$	$\frac{82889}{524892}$
0	2 1	$\frac{83}{250}$	$\frac{31}{50}$	$\frac{17}{20}$	\vdash	

Implicit, Fourth-order ESDIRK4

ESDIRK5





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Von Neumann Analysis

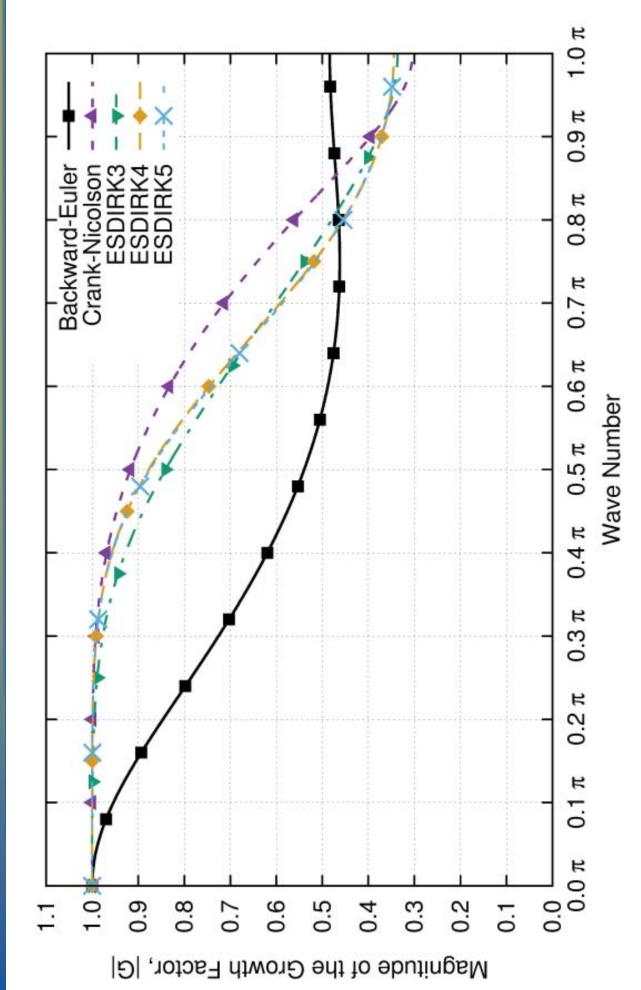


- Often used to study stability of schemes
- Von Neumann analysis is used to compare schemes for accuracy
- Dissipation error
- Dispersion error
- Assumes linear, periodic problems
- VNA theory and more results are in the associated paper



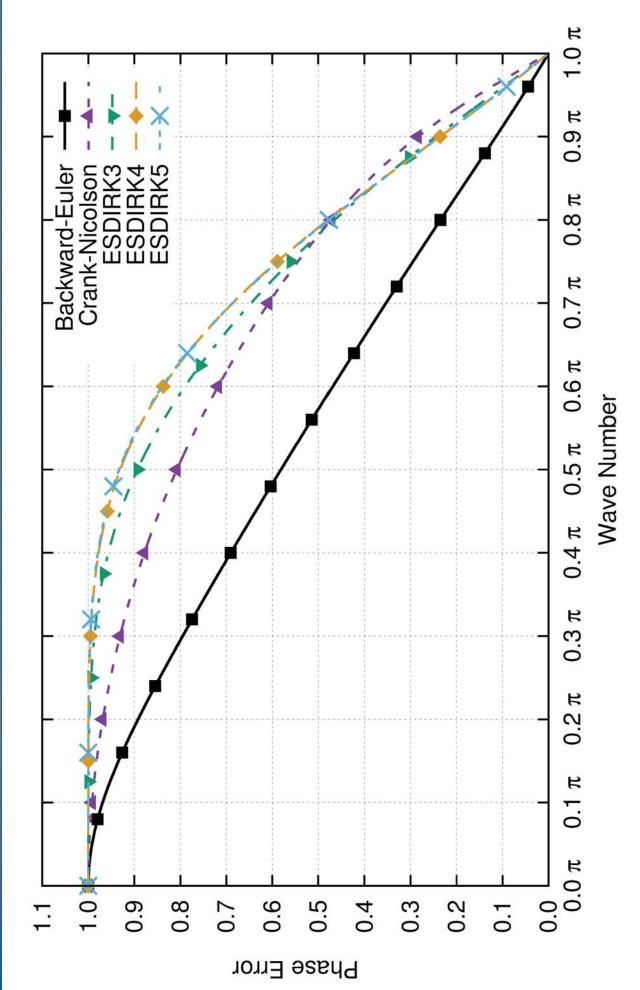
Dissipation, CFL = 1.0





Dispersion, CFL = 1.0



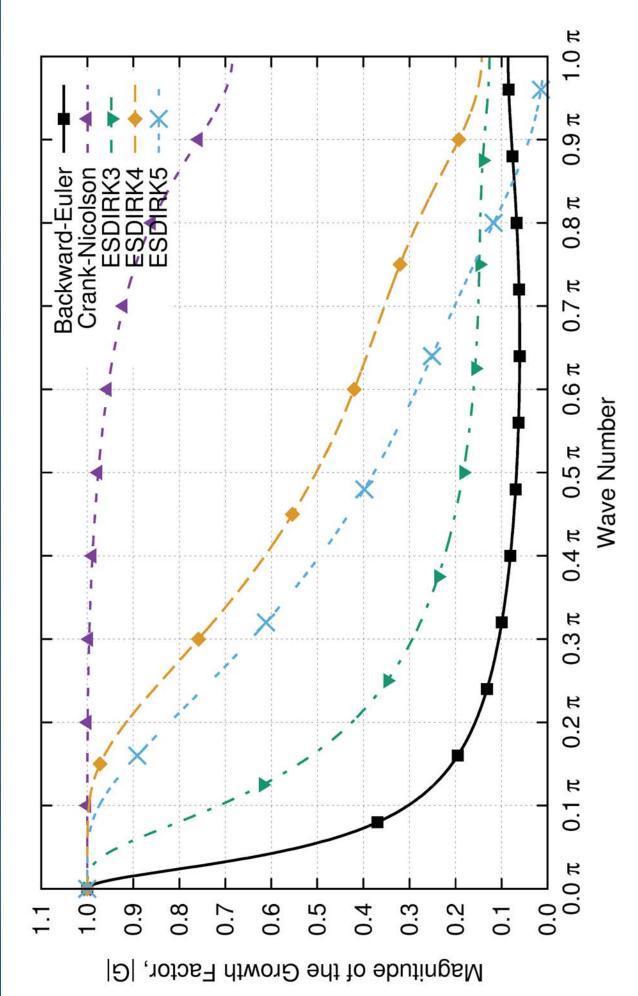


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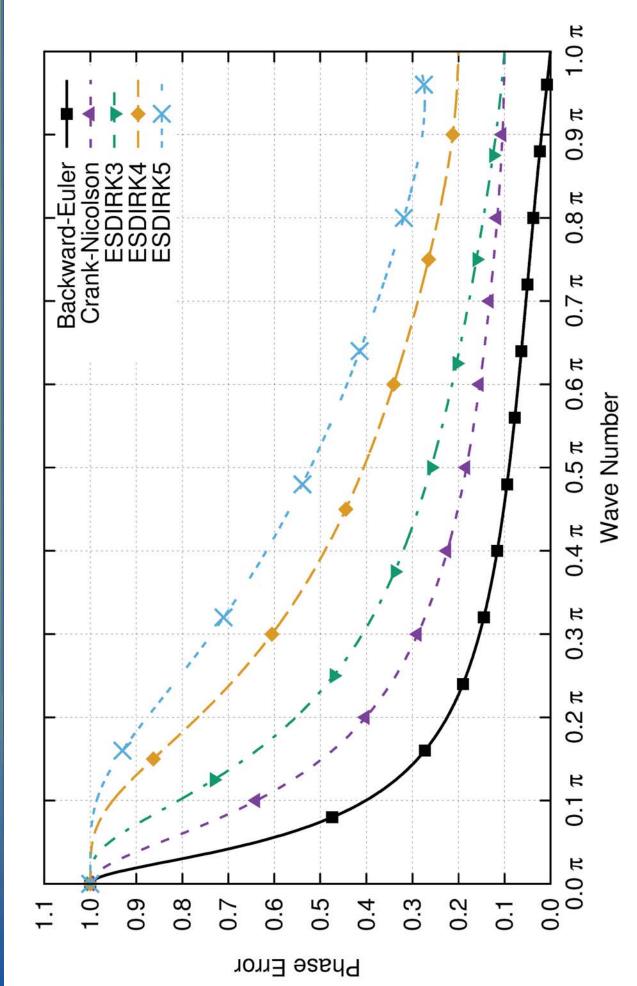
Dissipation, CFL = 10.0





Dispersion, CFL = 10.0





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1-D Acoustic Wave



Unperturbed Mach number of 0.5

$$\rho_{\infty} = 8.7077 \times 10^{-1} \frac{kg}{m^3}$$

$$\rho u_{\infty} = 1.7458 \times 10^2 \frac{kg}{m^2 \cdot s}$$

$$T_{\infty} = 400K$$

$$R_{\infty} = 2.871 \times 10^2 \frac{J}{kg \cdot K}$$

$$\gamma = 1.4$$

Perturbation wave - 20 points per wave resolution

$$Q_o = Q_{\infty} + M\delta\hat{Q}_{u,u\pm c}$$
$$\delta\hat{Q}_{u,u\pm c} = \hat{\delta} \cdot \cos(kx)$$
where $\hat{\delta} = 0.01$

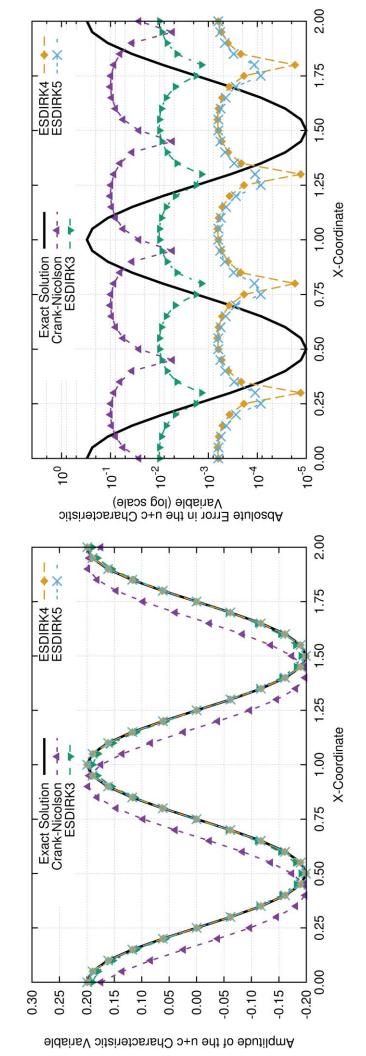
More results in the paper



1-D, CFL = 1.0, 10 Periods



	Dissipati	Dissipation Error	Dispersi	Dispersion Error
Scheme	VNA	Simulation	VNA	Simulation
Crank-N-colson	3.05×10^{-3}	3.05×10^{-3} 1.00×10^{-2}	8.11×10^{-2}	8.11×10^{-2} 8.11×10^{-2}
ESDIRK3	5.02×10^{-2}	5.02×10^{-2} 5.02×10^{-2} 1.51×10^{-3} 1.53×10^{-3}	1.51×10^{-3}	1.53×10^{-3}
ESDIRK4	3.13×10^{-3}	3.13×10^{-3} 3.13×10^{-3}	1.50×10^{-4}	1.50×10^{-4} 1.58×10^{-4}
ESDIRK5	3.14×10^{-3}	3.14×10^{-3} 3.14×10^{-3} 6.78×10^{-5} 6.90×10^{-5}	6.78×10^{-5}	6.90×10^{-5}

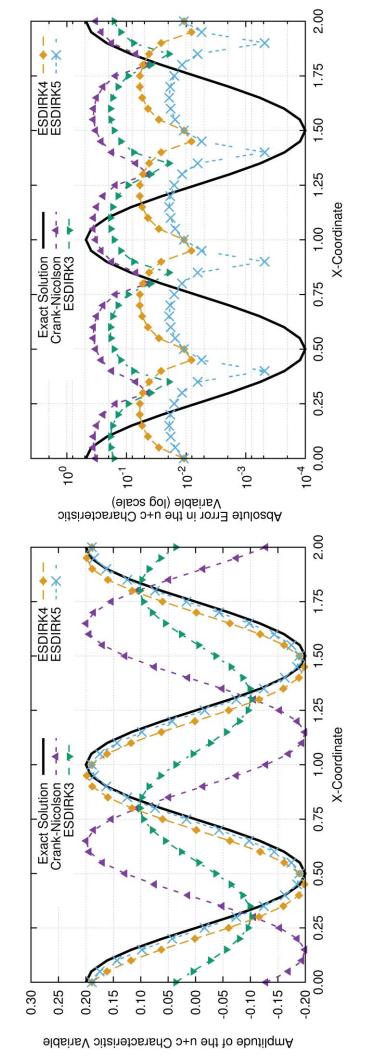




1-D, CFL = 10.0, 1 Period



	$\operatorname{Dissipati}$	Dissipation Error	$\operatorname{Dispersion}$	Dispersion Error
Scheme	VNA	Simulation	VNA	Simulation
Crank-Nicolson	9.02×10^{-5}	2.44×10^{-3}	3.61×10^{-1}	3.61×10^{-1}
ESDIRK3	4.99×10^{-1}	4.90×10^{-1}	1.92×10^{-1}	1.92×10^{-1}
ESDIRK4	7.22×10^{-3}	22×10^{-3} 7.25×10^{-3}	4.90×10^{-2}	4.90×10^{-2}
ESDIRK5	5.10×10^{-2}	5.46×10^{-2}	1.38×10^{-2}	1.39×10^{-2}

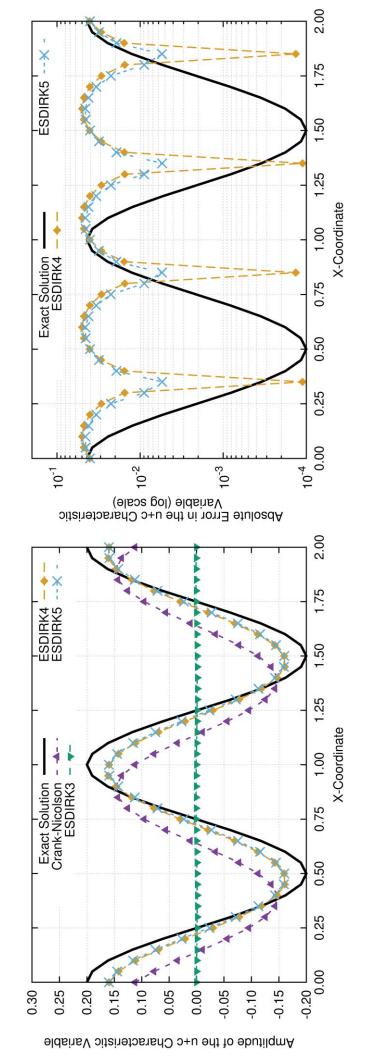




1-D, CFL = 1.0, 1000 Periods



	Dissipati	Dissipation Error	Dispersion	Dispersion Error
Scheme	VNA	Simulation	VNA	Simulation
Crank-Nicolson	2.63×10^{-1}	2.65×10^{-1}	8.11×10^{0}	8.10×10^{0}
ESDIRK3	9.94×10^{-1}	9.94×10^{-1}	1.51×10^{-1}	1.00×10^{-1}
ESDIRK4	2.69×10^{-1}	69×10^{-1} 1.95×10^{-1}	1.50×10^{-2}	3.00×10^{-2}
ESDIRK5	2.70×10^{-1}	70×10^{-1} 2.01×10^{-1}	6.78×10^{-3}	2.50×10^{-2}





3-D Isentropic Vortex



Free-stream Mach number of 0.5

$$\rho_{\infty} = 1.0 \frac{kg}{m^3}, \quad \rho u_{\infty} = 200.0 \frac{kg}{m^2 \cdot s}, \quad \rho v_{\infty} = 0.0 \frac{kg}{m^2 \cdot s}, \quad \rho w_{\infty} = 0.0 \frac{kg}{m^2 \cdot s}, \quad \rho e_{0,\infty} = 305714.3 \frac{kg}{m \cdot s^2}$$

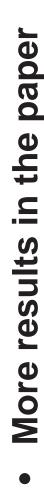
$$R_{\infty} = 287.11 \frac{J}{kg \cdot K}$$
 and $\gamma = 1.4$

Perturbation - 11 points across the vortex

$$\delta u = -\sqrt{R_{\infty}T_{\infty}} \frac{\alpha}{2\pi} (y - y_0) e^{\phi(1 - r^2)}$$

$$\delta v = \sqrt{R_{\infty} T_{\infty}} \frac{\alpha}{2\pi} (x - x_0) e^{\phi(1 - r^2)}$$

$$\delta T = T_{\infty} \frac{\alpha^2 \left(\gamma - 1 \right)}{16\phi \gamma \pi^2} e^{2\phi \left(1 - r^2 \right)}$$





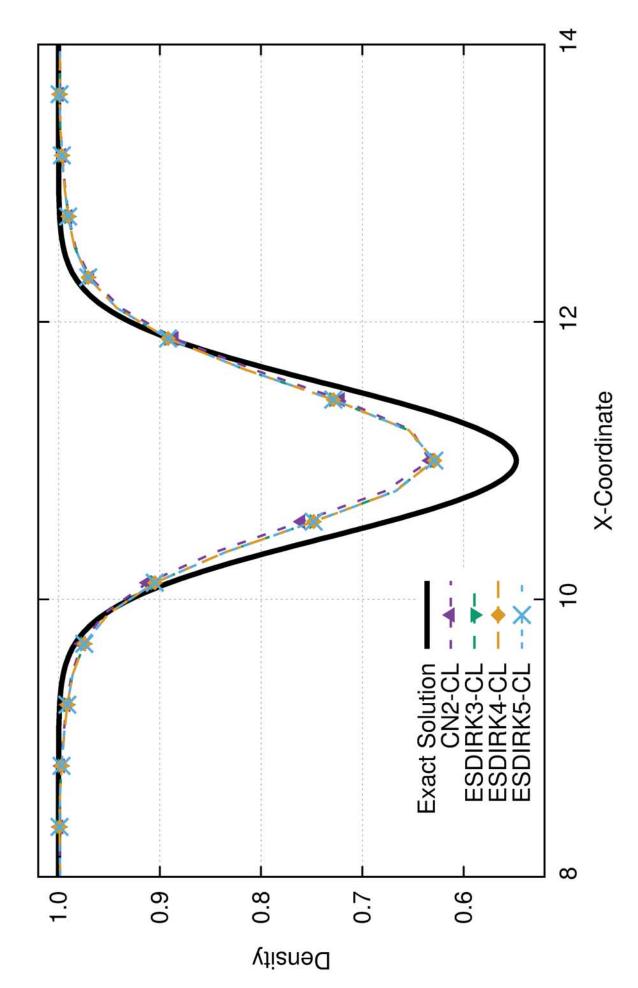
Vortex center: (x_0, y_0)





11 Points Across the Vortex 3-D, CFL = 1.0, 40 Lengths,





2-2

2-3

5₋0

1.04

dx (log scale)

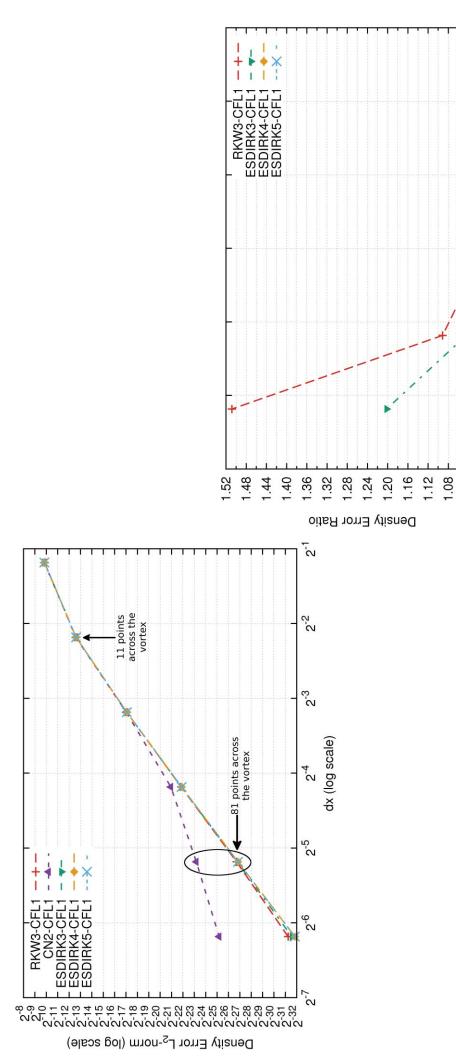
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Different Resolutions

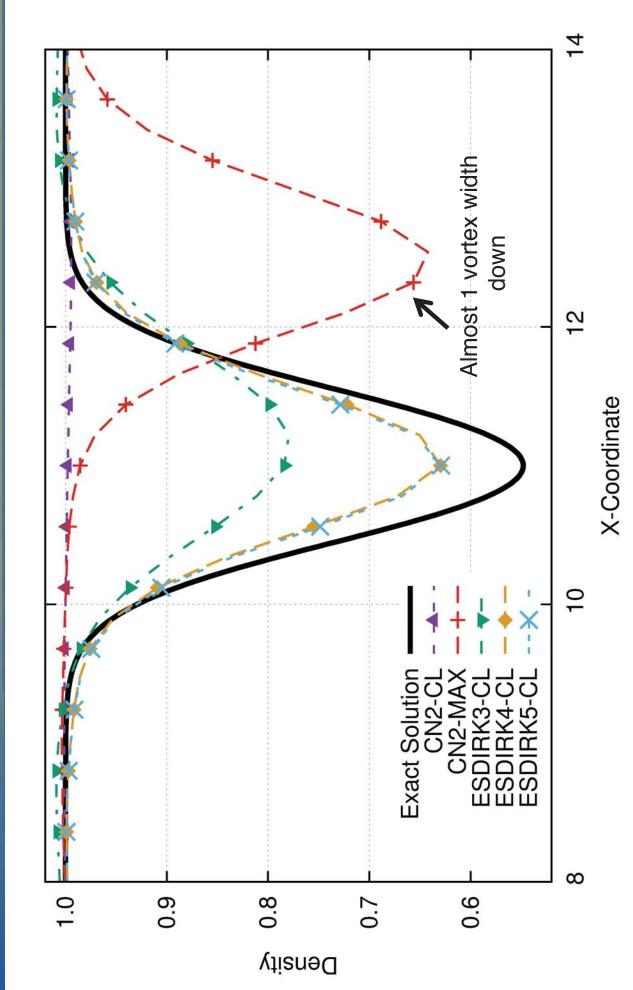






11 Points Across the Vortex 3-D, CFL = 8.0, 40 Lengths,



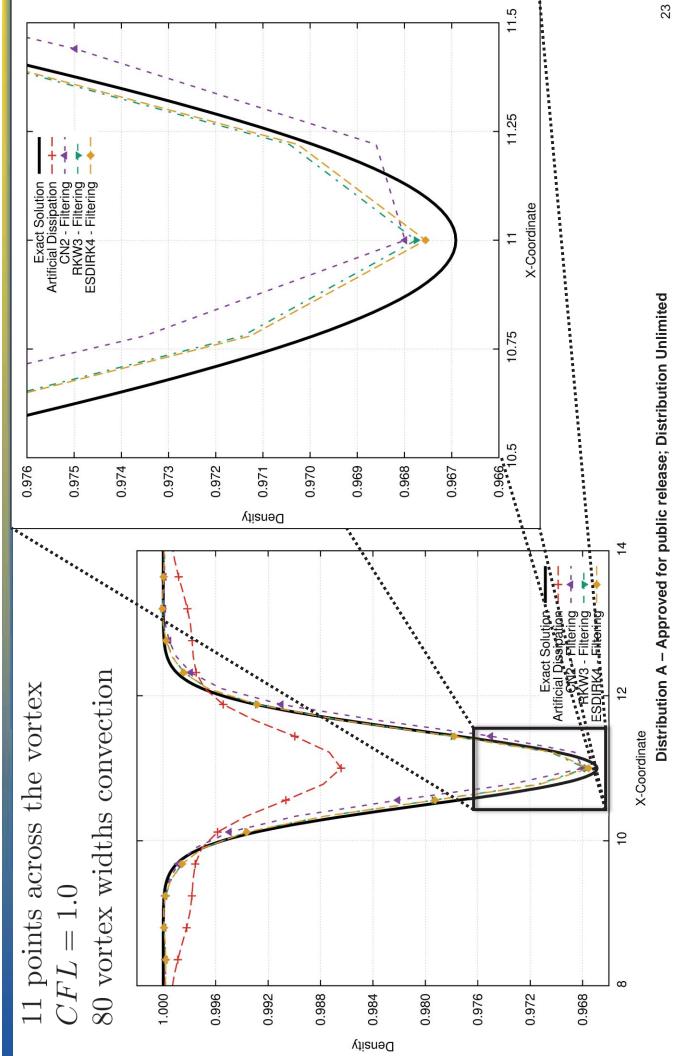


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Sneak Peak: Filtering





Conclusions



2nd- and 3rd-order time integrators for 5th-order spatial schemes are inadequate

- The same order of spatial and temporal discretizations is preferable
- However, ESDIRK5 is not much better than ESDIRK4
- 7 implicit stages vs. 5 implicit stages

Higher-order time integrators:

- Do not show significant improvement on coarse grids at CFL of one
- Are better at high CFL number
- Are better on highly refined grids

Spatial error usually dominates for typical CFL numbers and grid resolutions

Central difference plus artificial dissipation schemes are inadequate

Future Work

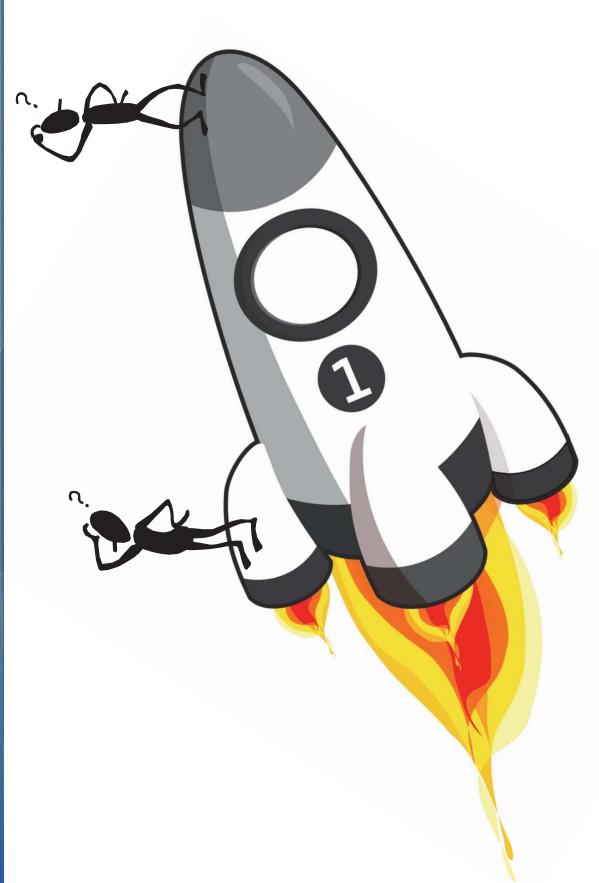


- Implement more accurate spatial schemes of the same orders of accuracy
- Compact-difference schemes
- Filtering schemes
- desired dissipation and dispersion properties Derive better ESDIRK schemes tailored to the
- advantage of the ESDIRK time integrators for Add preconditioning to take maximum stiff problems
- Improved convergence efficiency
- Improved solution accuracy

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Questions???





Extra Slides



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3-D, CFL = 8.0Different Resolutions

